

# Viscous Dissipation Inside Electric Motors

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**Abstract** - A numerical study has been carried out to quantify the level of viscous dissipation inside an electrical motor. The study has been performed using an in-house computational model. This paper presents the effect of several geometrical and operating parameters on the level of viscous dissipation generated within the stator-rotor gap. The geometrical parameters considered in this study are the gap size and the stator inner diameter, varied in the range of 0.25-1.4 mm and 55-375 mm, respectively. The operating parameter considered in this study is the rotor rotational speed, which was varied in the range of 900-3600 rpm. The numerical results have been validated using experimental data. Results indicated that the amount of heat generated due to viscous dissipation is directly proportional to the stator diameter and rotor rotational speed, and inversely proportional to the gap thickness.

**Keywords:** Viscous dissipation, Electric motors, Taylor Couette flow, Thermal performance.

## 1. Introduction and Literature Review

A typical electric motor consists of several components shown in Fig. 1. The main components are the stator and rotor within which a gap is present. Electric motors generate heat losses due to electric current passing through the motor windage resistance and due to viscous dissipation within the rotor-stator gap. The gap thickness and the stator inner diameter could dramatically affect the amount of heat generated due to viscous dissipation especially if the gap is filled with a high viscosity lubricating fluid. To minimize the possibility of electric motors overheating, the motor design should be focused on minimizing the total amount of heat losses generated within the motor.

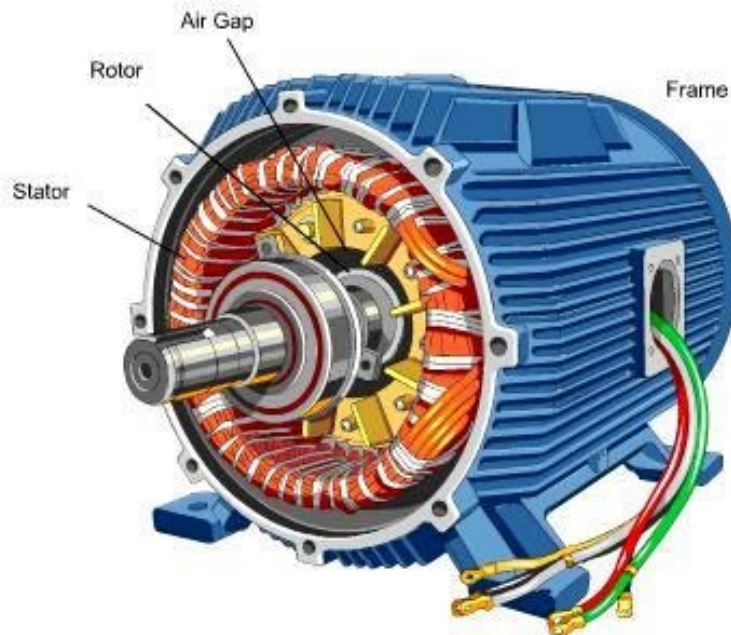


Fig. 1: Electrical motor main components [1].

The flow of the lubricating fluid within the rotor-stator gap is commonly referred to as a Taylor-Couette flow because the typical Taylor-Couette flow is a flow between two concentric cylinders. Many researchers have investigated the Taylor-Couette flow. The work reported in [2], [3], [4], [5] and [6] was focused on the heat transfer and fluid flow of a single-phase Taylor-Couette flow considering the stability of such flow. The previous studies showed that, the increase in the rotational speed enhanced the heat transfer inside the gap. A review of flow between two concentric cylinders was reported in [7]. [8] investigated a multi-phase Taylor-Couette flow of air and oil within two concentric cylinders. This study proved that the optimum oil volume percentage was 65% for heat transfer inside the gap. The higher the rotational speed, the higher the rate of heat transfer inside the gap. [9] studied the effect of adding a set of longitudinal slots along the outer concentric cylinder. The slots studied were rectangular, trapezoidal and elliptical in shape. The elliptical shaped slots gave the best heat transfer behaviour. [10] studied transient heat transfer inside a motor gap. To the best of the authors' knowledge, there has not been any studies of the effect of gap size and rotational speed on the level of viscous dissipation within a motor gap.

## 2. Problem Definition

The problem of interest involves the estimation of heat generated due to viscous dissipation within the rotor-stator gap of an electric motor shown in Fig. 2. The gap length is 140 mm. The rotor is rotating at a constant speed ( $N$ ). All solid surfaces are assumed smooth. The gap is filled with an Enduratex EP150 oil. The oil properties were taken from the material data sheet reported in [11]. The motor is fully submerged in oil.

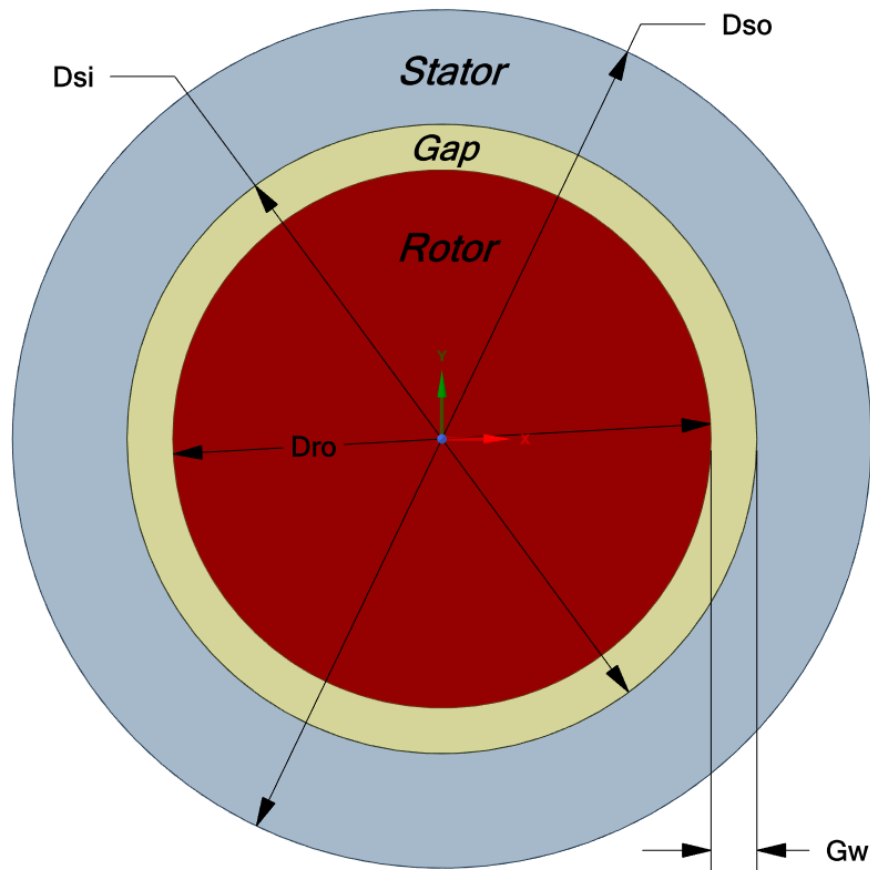


Fig. 2: Schematic diagram of the current problem

### 3. Mathematical Model

An in-house numerical model has been used to estimate the amount of viscous dissipation developed with the gap. The amount of viscous dissipation ( $P_w$ ) has been calculated using equation (1) from [12]. The skin friction coefficient ( $C_d$ ) was calculated from equation (2) using an iterative method. Reynolds number ( $Re$ ) is defined in equation (3) using the gap thickness as the characteristic length scale. The stator was assumed insulated, and the rotor was assumed rotating with a constant rotational speed.

$$P_w = \pi C_d \rho R_r^4 \omega^3 L \quad (1)$$

$$\frac{1}{\sqrt{C_d}} = 2.04 + 1.768 \ln(Re \sqrt{C_d}) \quad (2)$$

$$Re = \frac{\omega R_r \rho G_w}{\mu} \quad (3)$$

The variables included in equations (1)-(3) are defined as follows:

$P_w$  is the heat rate generated due to viscous dissipation in W.

$C_d$  is the skin friction coefficient.

$\rho$  is the oil density in  $\text{kg/m}^3$  and is calculated at the average oil temperature within the gap.

$R_r = \frac{D_{ro}}{2}$  is the rotor outer radius in m.

$\omega = \frac{2\pi N}{60}$  is the rotor angular velocity in rad/sec.

$L$  is the rotor length in m.

$Re$  is the Reynolds number.

$G_w$  is the gap width in m and is defined as shown in Fig. 2.

$\mu$  is the dynamic viscosity of oil in Pa.sec and is calculated at the average temperature across the gap.

### 4. Validation of The Numerical Results

Validation of the present numerical results has been carried out using experimental and numerical data reported in [12]. [12] studied viscous dissipation inside a motor gap filled with air. The length and radius of the rotor were 0.1142 m and 0.1 m, respectively. The gap width was 0.63 mm. The rotor rotational speed was varied from 3600 rpm to 12000 rpm. The corresponding Reynolds number ( $Re$ ) ranged from 1500 to 5000. The maximum deviation found between the present numerical results and the data reported in [12] is about 3.5%, as illustrated in Fig. 3.

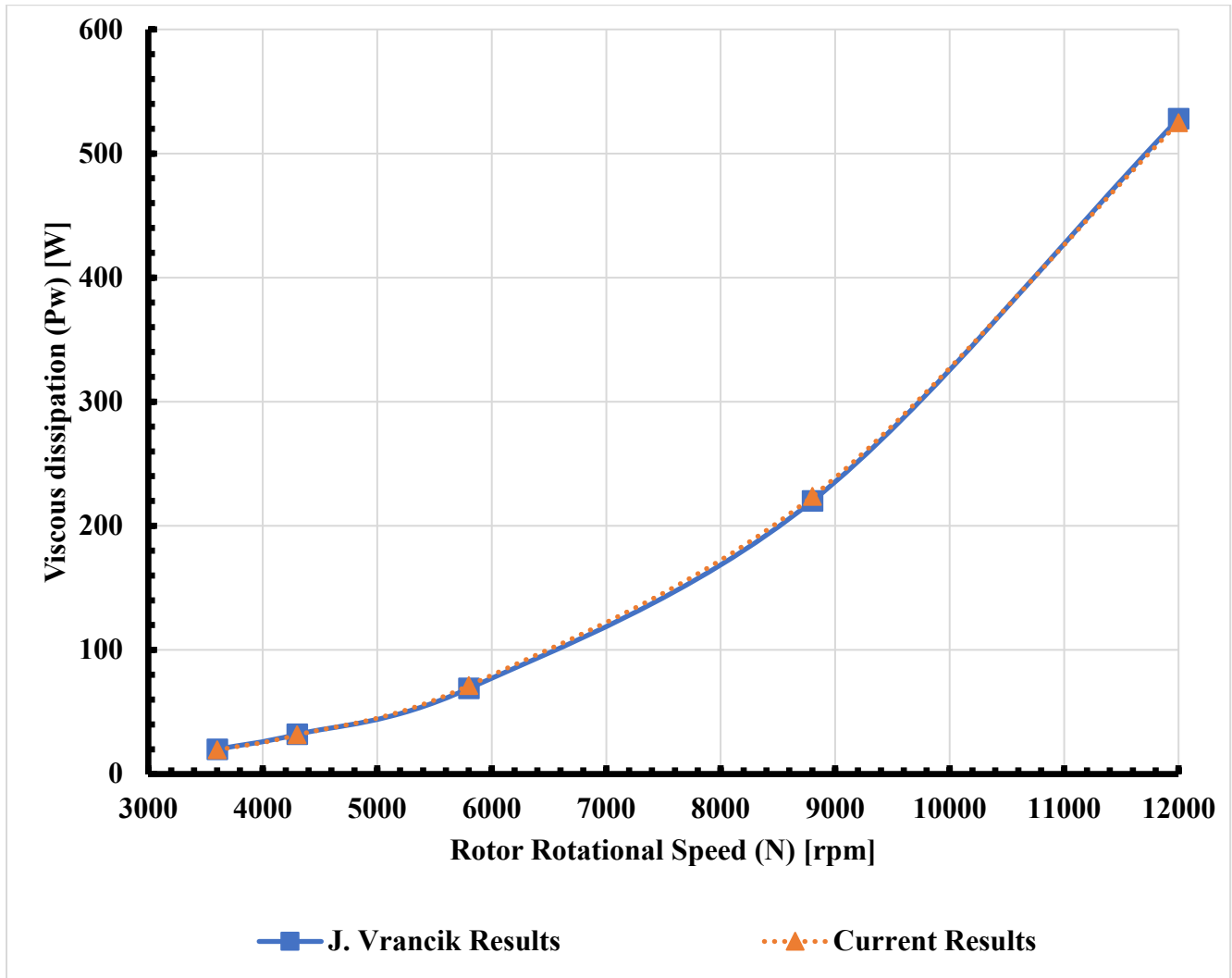


Fig. 3: Validation of current numerical results with results reported in [12].

## 5. Results and discussion

The parameters investigated in the present study are the gap size [ $G_w$ ], the stator inner diameter [ $D_{si}$ ] and the rotor rotational speed [ $N$ ]. These parameters have been varied in the ranges of 0.25-1.4 mm, 55-375 mm and 900-3600 rpm, respectively. The effect of these parameters on viscous dissipation [ $P_w$ ] has been investigated.

### 5.1. Effect of gap size on viscous dissipation

Fig. 4 shows the effect of the gap size on the viscous dissipation at constant stator inner diameter of 55 mm and rotor rotational speed of 3600 rpm. Results indicate that the increase in gap size reduces the viscous dissipation where the best gap thickness is the largest of 1.4 mm. That is explained from equation (3) as the Reynolds number ( $Re$ ) is increased with increasing the gap size. Hence, the skin friction factor ( $C_d$ ) is reduced as from equation (2) and in return the viscous dissipation is decreased as from equation (1). The rate of reduction in the viscous dissipation is not a linear relation due to the fact of that the skin friction factor ( $C_d$ ) is not directly proportional with the Reynolds number ( $Re$ ).

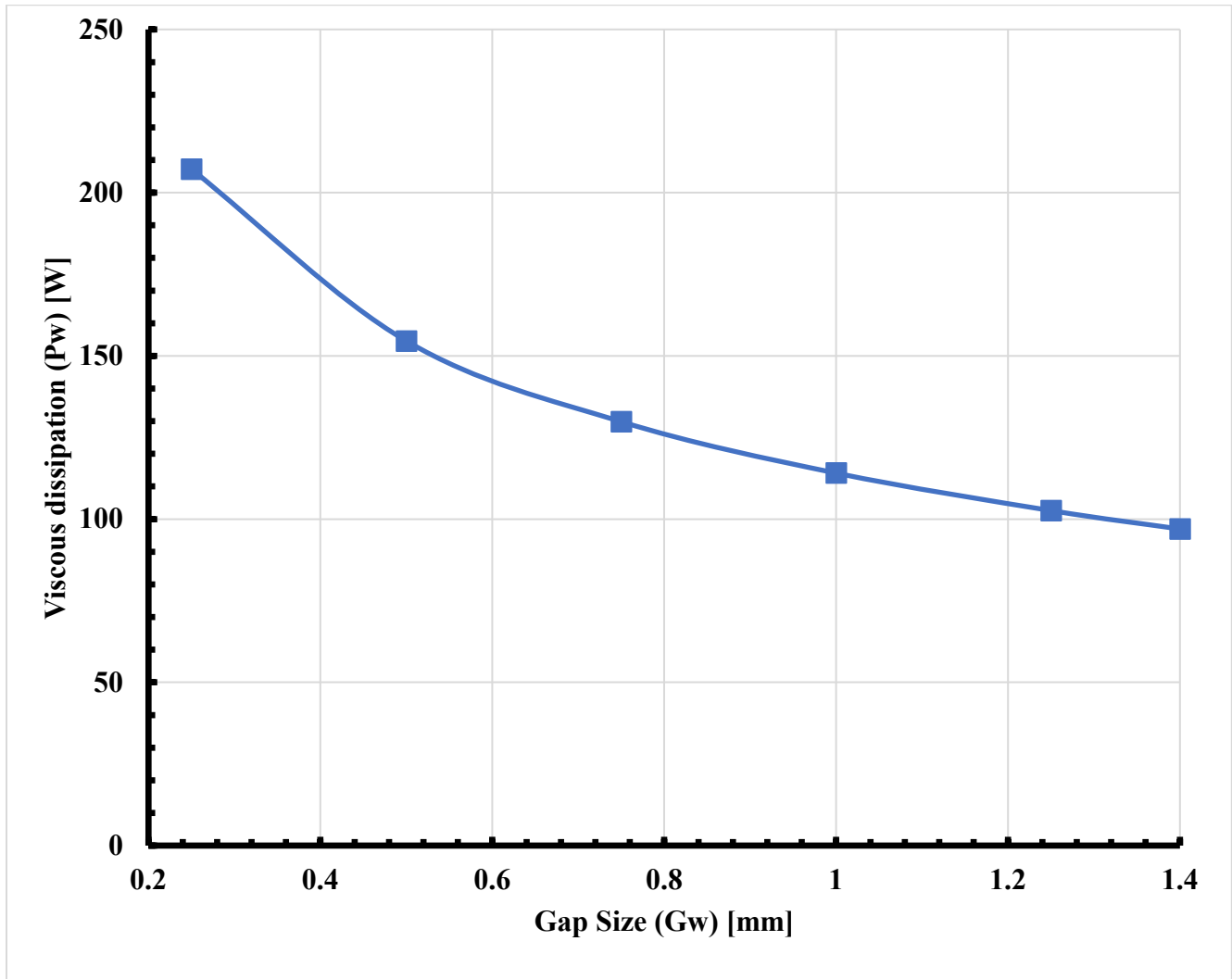


Fig. 4: Effect of gap size on viscous dissipation at  $N = 3600$  rpm and  $D_{si} = 55$  mm.

## 5.2. Effect of stator inner diameter on viscous dissipation

Fig. 5 shows the effect of the stator inner diameter on the viscous dissipation at constant gap size of 1.4 mm and rotor rotational speed of 3600 rpm. The results showed that with increasing the stator inner diameter ( $D_{si}$ ), the viscous dissipation increased dramatically. The viscous dissipation is increased as from equation (1) as the rotor radius ( $R_r$ ) is raised to the power of 4. The increase in the rotor radius ( $R_r$ ) increases the Reynolds number which reduces the skin friction factor ( $C_d$ ). However, the effect of the skin friction factor ( $C_d$ ) is not dominant in changing the viscous dissipation as it is just raised to the power of 1. So, the dominant parameter in the calculations of the viscous dissipation is the stator and rotor radius.

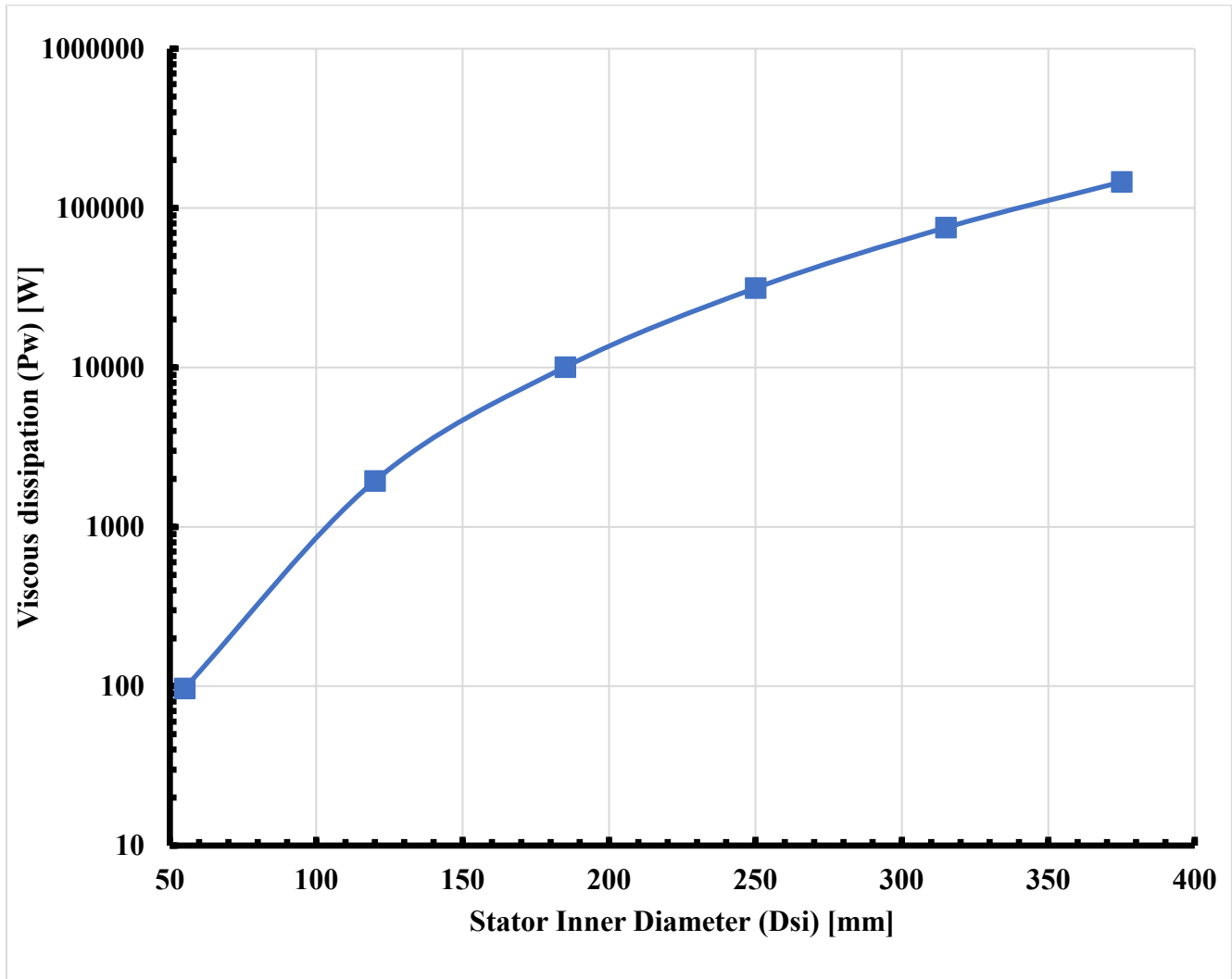


Fig. 5: Effect of stator inner diameter on viscous dissipation at  $N = 3600$  rpm and  $G_w = 1.4$  mm.

### 5.3. Effect of rotor rotational speed on viscous dissipation

Fig. 6 shows the effect of the rotor rotational speed on the viscous dissipation at constant gap size of 1.4 mm and stator inner diameter of 55 mm. Results indicated that the increase in the rotor rotational speed increases the viscous dissipation inside the motor gap. As shown in Fig. 6 the highest rotor rotational speed of 3600 rpm has the largest amount of viscous dissipation. As clear from equation (1), the increase in the rotor rotational speed increases the viscous dissipation significantly as the angular velocity ( $\omega$ ) is raised to the power 3.

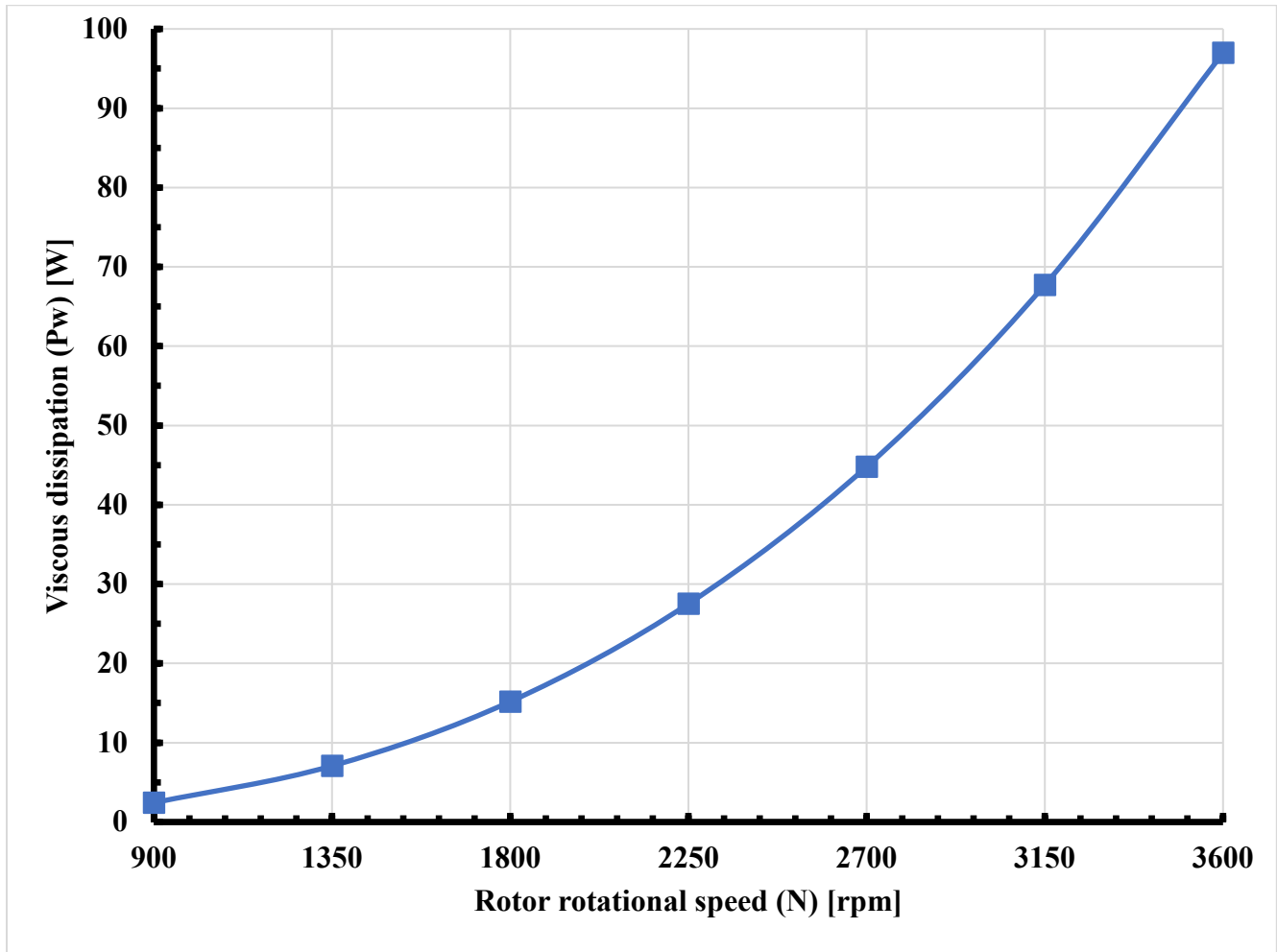


Fig. 6: Effect of rotor rotational speed on viscous dissipation at  $D_{si} = 55$  mm and  $G_w = 1.4$  mm.

## 6. Conclusion

The paper covered the effect of multiple geometrical and operational parameters on the amount of viscous dissipation inside the motor gap. One can easily note that increasing the gap size reduced the viscous dissipation inside the gap. Also, the reduction in the rotor radius and rotor rotational speed decreased viscous dissipation within the motor gap. The most dominant parameter is the rotor radius as a small change (increase) in the rotor radius resulted in a significant change (increase) in viscous dissipation.

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