

Organosolv Modified Wheat Straw as Adsorbent for Basic Dyes in Water Bodies

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Abstract - Biomass and especially lignocellulosic residues offer a low-cost and renewable additional source of adsorbents and can be used as is or modified or transformed to activated carbon. These waste materials have little or no economic value and often present a disposal problem. Therefore, there is a drive to valorize these low-cost by-products. Various low-cost adsorbents from agricultural by-products have been studied to remove dyes from aqueous solutions. In this work, a sulfuric acid-catalyzed organosolv pretreatment process using five organic solvents, i.e., ethanol, methanol, diethylene glycol, acetone and butanol, was applied to modify wheat straw under carefully selected conditions. The low-cost material, i.e., modified wheat straw was used as adsorbent for cleaning of water bodies' pollution. The potentiality of modified wheat straw for the adsorptive removal of Methylene Blue (MB), a representative basic dye, from aqueous solutions was studied. The experimental batch adsorption system data were simulated using (a) Freundlich, Langmuir and Sips isotherm models and (b) first order, second order and intraparticle diffusion kinetic models.

Keywords: adsorption, methylene blue, organosolv, pretreatment, sulfuric acid, wheat straw

1. Introduction

The contamination of water due to color effluents coming from different industries is a current problem all over the world [1]. Textile dyes and other industrial dyestuffs form one of the largest groups of organic compounds that represent an increasing environmental danger by releasing toxic and potential carcinogenic substances into the aqueous phase. Textile industry requires about 700,000 t of different types of dyes for the annually world production [2]. Textile industries wastewater is known to contain considerable amounts of non-fixed dyes, azo dyes, and a quantity of inorganic salts. The most of the dyes used in dyeing processes are released into the environment, which causes considerable environmental pollution problems [1]. Therefore, many methods are available for the removal of dyes from industrial effluents. The most widely used are biodegradation [3], flocculation-coagulation [4], chemical oxidation [5] and adsorption. Among these methods, the adsorption technique has been proven to be effective and attractive for the treatment of dye-bearing wastewaters [6].

During the past decades, activated carbon (AC) is the most commonly used adsorbent. However, the AC suffers from some drawbacks such as high cost, difficult disposal and regeneration [7]. Recently, increasing attention was paid on the development of highly effective and low cost adsorbents [8-10]. In this respect, renewable adsorbents are attractive because of their low cost, easy availability and low toxicity. Various renewable materials, such as peanut husk [11], wheat straw [12], cotton stalk [13], sugar beet pulp [14], pistachio hull [15], papaya seeds [16], and fruit peel [17], have been used as adsorbent for the removal of dye from aqueous solution.

In this work, the removal of MB by wheat straw modified by sulfuric acid catalyzed organosolv pretreatment was studied using untreated wheat straw as control. The adsorption isotherms and adsorption kinetics of MB were used to estimate and compare the adsorption capacity of the untreated and pretreated wheat straw.

2. Materials & Methods

Wheat straw sulfuric acid-catalyzed organosolv pretreatment process with (i) ethanol, (ii) methanol, (iii) diethylene-glycol, (iv) acetone and (v) butanol as organic solvent was used to produce adsorbents for methylene blue cleaning. The organosolv pretreatment process was performed in a 3.75-L batch reactor PARR 4843. The isothermal treatment times was

20 and 40 min (not including the non-isothermal preheating and the cooling time-periods); the reaction was catalyzed by sulfuric acid and organic acids produced by the wheat straw during the reaction conditions; the liquid-to-solid ratio was 20:1; the liquid phase volume was 2000 mL, i.e., 1000 mL organic solvent and 1000 mL water; the solid material dose was 100 g; the stirring speed 150 rpm. The reaction ending temperature values were 160°C and 180°C, reached after 42 and 62 min preheating time values, respectively.

The dye used in batch experiments was Methylene Blue produced by Allfa Aesar GmbH and Co KG, Karlsruhe, Germany. MB has a chemical formula of $C_{16}H_{18}ClN_3S \cdot xH_2O$ with molecular weight of $319.86 \cdot 10^{-3} \text{ kg mol}^{-1}$. A stock solution was prepared by dissolving 5 g of MB in 25 L distilled water. Working solutions were 1.6-156 mg L^{-1} . MB concentrations were analyzed by measuring the absorbent values in each experiment with a HACH LANGE DR6000 spectrophotometer at $\lambda=664 \text{ nm}$.

Isotherms were obtained from batch experiments. After the batch process, weigh accurately the quantities of tissue were transferred to 0.8-L bottles, where $V = 0.5 \text{ L}$ adsorbate solution were added. The adsorbent weight was 0.5 g, the temperature was $T = 23^\circ\text{C}$, the original MB concentration ranged from $C_0 = 1.6 \text{ mg L}^{-1}$ to 156 mg L^{-1} . The bottles were sealed and mechanically filled for a period of 7 days. This time period was chosen after pilot studies (the time varies from 4 hours to 14 days) to ensure that nearly equilibrium conditions are achieved. The resulting solution was determined concentrations and balance data from each bottle represented one point on the adsorption isotherm plots. The values of solution pH were near 8.

As regards the accuracy of the results the Mean Average Percentage Error was 0.39% for kinetic experiments and 1.2% for isotherm experiments.

Adsorption rate batch experiments were conducted in a 2-L glass totally mixed reactor equipped with a twisted blade agitator type, operating at 600 rpm, for maintaining the lignocellulosic material in suspension. The reactor, containing $V = 1 \text{ L}$ aqueous solution of dye was placed in a water bath to maintain constant temperature at the desired level. The adsorbent mass was $m = 1 \text{ g}$, the temperature was 23°C , the initial concentration of MB was $C_0 = 14 \text{ mg L}^{-1}$.

3. Results & Discussion

The comparison of the adsorption capacity of the seaweed samples was based on the Freundlich [18], Langmuir [19] and Sips [20] isotherm models. The first two models are both widely used for investigating the adsorption of a plethora of dyes on various lignocellulosic materials and activated carbons. The Freundlich [18] isotherm is given by the following equation:

$$q = K_F \cdot (C_e)^{\frac{1}{n}} \quad (1)$$

where q is the amount adsorbed per unit mass of the adsorbent (mg g^{-1}), C_e is the equilibrium concentration of the adsorbate (mg L^{-1}) and $K_F [(\text{mg g}^{-1})(\text{L mg}^{-1})^{1/n}]$, n are the Freundlich constants related to adsorption capacity and intensity, respectively. The K_F and n values were estimated by non-linear regression analysis (NLRA) from the experimental adsorption data obtained at 23°C for MB. The standard error of estimates (SEE)-values was calculated by the following equation:

$$SEE = \sqrt{\sum_{i=1}^n (y_i - y_{i,theor})^2 / (n' - p')} \quad (2)$$

where: y_i is the experimental value of the depended variable, $y_{i,theor}$ is the theoretical (estimated) value of the depended variable, n' is the number of the experimental measurements and p' is the number of parameters, i.e., $(n' - p')$ is the number of the degrees of freedom. The parameters of the Freundlich adsorption model can be obtained by NLRA.

The Langmuir isotherm equation [19] is based on the following ‘pseudo-monolayer’ adsorption model.

$$q = \frac{K_L q_m C_e}{1 + K_L C_e} \quad \text{or} \quad \frac{1}{q} = \left(\frac{1}{q_m} \right) + \left(\frac{1}{K_L \cdot q_m} \right) \cdot \left(\frac{1}{C_e} \right) \quad (3)$$

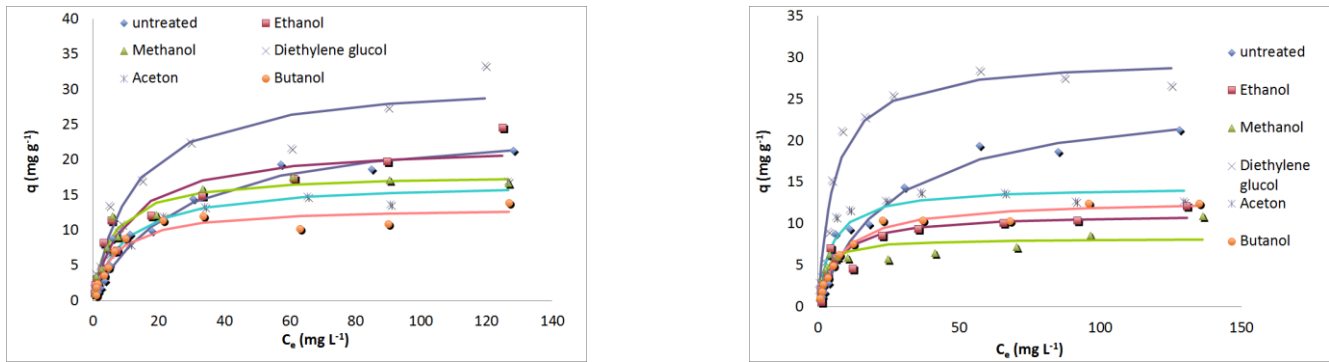


Fig. 1: Langmuir isotherms for MB adsorption on modified wheat straw at 160 °C for 20 min (left) and 40 min (right).

Table 1: Parameters of Freundlich and Langmuir isotherm models of Methylene Blue adsorption on modified wheat straw.

Pretreatment	Freundlich isotherm model			Langmuir isotherm model		
	K_F	n	SEE	q_m	K_L	SEE
Untreated	2,79	2,28	2,12	25,65	0,0392	1,51
160°C, 20min						
Ethanol	3,98	2,71	1,80	22,26	0,0987	2,32
Methanol	4,82	3,46	2,29	18,07	0,1731	1,27
Diethylene glycol	5,14	2,60	2,58	31,67	0,0836	2,71
Acetone	3,38	2,92	2,01	16,94	0,1045	1,15
Butanol	3,28	3,31	2,01	13,27	0,1483	1,17
160°C, 40min						
Ethanol	2,86	3,31	1,42	11,27	0,1585	1,37
Methanol	3,14	4,37	1,17	8,24	0,4068	1,25
Diethylene glycol	8,02	3,47	4,63	30,06	0,1785	1,86
Acetone	4,52	3,94	2,72	14,53	0,2106	1,41
Butanol	2,95	3,19	1,34	12,93	0,1207	0,55
180°C, 20min						
Ethanol	3,43	3,74	1,95	11,78	0,1824	1,19
Methanol	2,12	3,85	1,23	6,86	0,2016	1,09
Diethylene glycol	4,26	2,92	2,31	20,67	0,1196	2,39
Acetone	2,74	2,27	1,85	23,49	0,0527	2,32
Butanol	1,45	1,97	1,66	20,20	0,0273	2,01

where K_L is the Langmuir constant related to the energy of adsorption ($L \text{ mg}^{-1}$) and q_m the amount of dye adsorbed (mg g^{-1}) when saturation is attained. In cases where the isotherm experimental data approximates the Langmuir equation, the parameters K_L and q_m can be estimated either by plotting $1/q$ versus $1/C_e$ either by NLRA.

The Sips (Langmuir – Freundlich) [20] isotherm equation, also examined in the present work, is based on the following adsorption model:

$$q = \frac{q_m \cdot (K_L \cdot C_e)^{1/n}}{1 + (K_L \cdot C_e)^{1/n}} \quad (4)$$

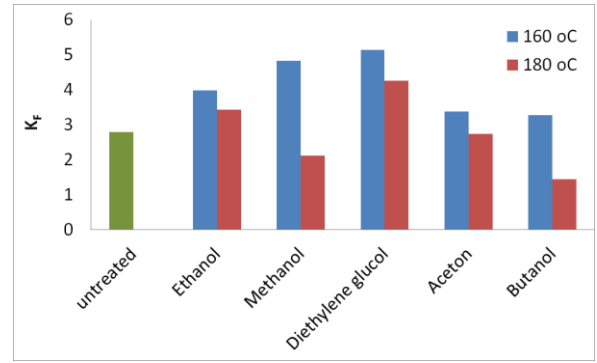
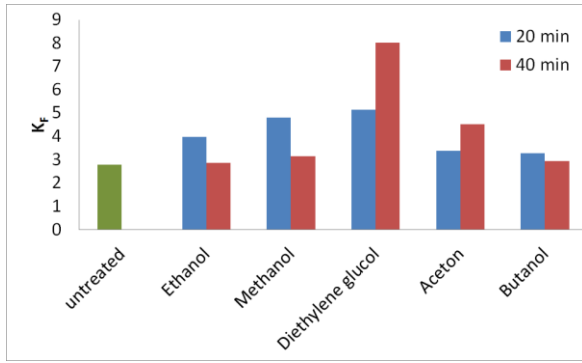


Fig. 2: Isotherm parameter K_F according to the Freundlich model of MB adsorption on modified wheat straw at 160 °C for 20 min and 40 (left) and at 160 and 180 °C for 20 min (right).

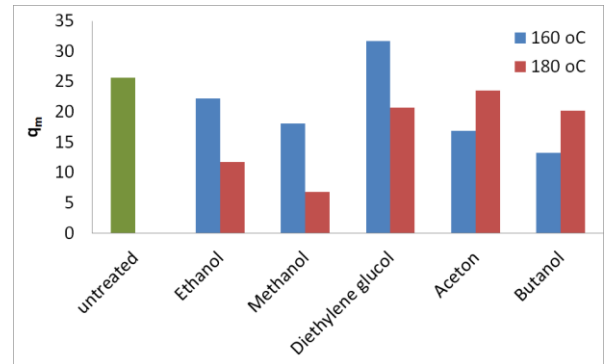
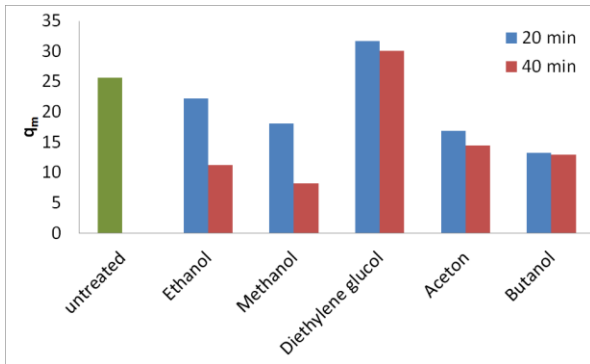


Fig. 3: Isotherm parameter q_m according to the Langmuir model of MB adsorption on modified wheat straw at 160 °C for 20 min and 40 (left) and at 160 and 180 °C for 20 min (right).

where K_L , q_m is the Langmuir constants and n the Freundlich constant.

The fitting of the Langmuir's adsorption model to the MB adsorption experimental data was satisfactory as can be seen in Fig.1. In Table 1 the estimated parameter values and the SEE for Freundlich and Langmuir isotherms are presented. The low SEE values prove the good fitting of these models on the experimental data. In Fig. 3 the Freundlich isotherm-parameter K_F values estimated using NLRA are presented. Similarly, in Fig. 4 the Langmuir isotherm-parameters q_m estimated using NLRA are presented.

Kinetic models' equations: The kinetics of adsorption of MB on various materials has been extensively studied using three kinetic equations. The widely used Lagergren equation [21] is shown below:

$$q - q_t = q \cdot e^{-k \cdot t} \quad (5)$$

where q and q_t are the amounts of MB adsorbed per unit mass of the adsorbent (in mg g^{-1}) at equilibrium time ($t \rightarrow \infty$) and adsorption time t , respectively, while k is the pseudo-first order rate constant for the adsorption process (in min^{-1}). Furthermore, $q = (C_0 - C_e)V/m$ and $q_t = (C_0 - C)V/m$ where C , C_0 , C_e are the concentrations of MB in the bulk solution at time t , 0, and ∞ , respectively, while m is the weight of the adsorbent used (in g), and V is the solution volume (in mL). The commonly used second-order kinetic model [22] is as follows:

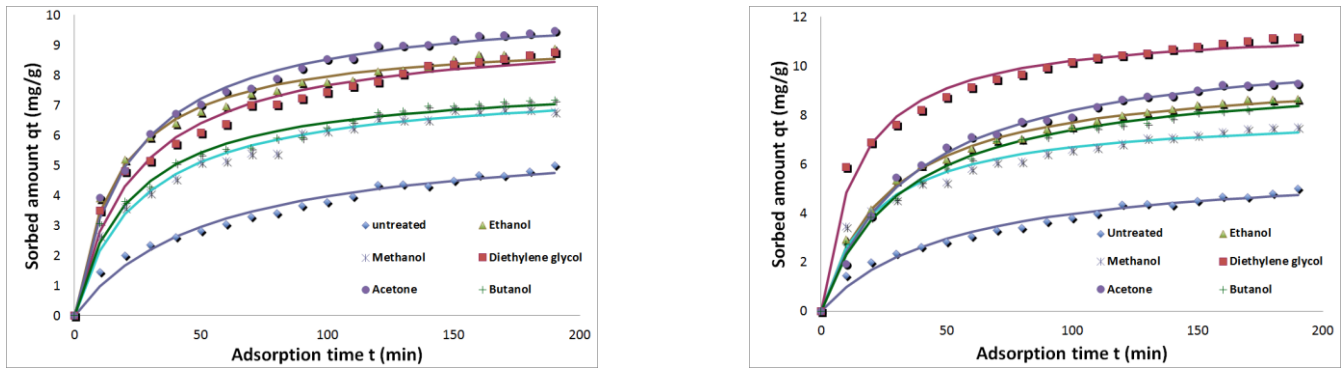


Fig. 4: Kinetics according to the second order model of MB adsorption on modified wheat straw at 160 °C for 20 min (left) and 40 min (right).

Table 2: Parameters of 1st and 2nd order kinetic models for Methylene Blue adsorption on modified wheat straw.

Pretreatment	1 st order kinetic model			2 nd order kinetic model		
	k (min^{-1})	q (mg g^{-1})	SEE	k ($\text{g mg}^{-1} \text{min}^{-1}$)	q (mg g^{-1})	SEE
Untreated	0.0184	4.80	0.270	0.0032	6.045	0.199
160°C, 20min						
Ethanol	0.0420	8.23	0.471	0.0063	9.310	0.215
Methanol	0.0303	6.63	0.365	0.0050	7.750	0.214
Diethylene glycol	0.0316	8.19	0.523	0.0044	9.510	0.302
Acetone	0.0343	9.02	0.462	0.0044	10.412	0.225
Butanol	0.0334	6.81	0.418	0.0056	7.873	0.241
160°C, 40min						
Ethanol	0.0301	8.30	0.358	0.0038	9.789	0.147
Methanol	0.0346	7.06	0.469	0.0059	8.092	0.276
Diethylene glycol	0.0474	10.46	0.672	0.0061	11.650	0.338
Acetone	0.0254	9.11	0.272	0.0025	11.127	0.192
Butanol	0.0265	8.16	0.314	0.0031	9.803	0.159
180°C, 20min						
Ethanol	0.0073	11.76	0.211	0.0003	18.571	0.226
Methanol	0.0242	7.65	0.368	0.0030	9.240	0.234
Diethylene glycol	0.0524	9.36	0.607	0.0078	10.352	0.298
Acetone	0.0110	11.62	0.193	0.0005	16.980	0.242
Butanol	0.0137	8.69	0.096	0.0009	12.080	0.164

$$q_t = q - [q^{-1} + k_2 t]^{-1} \quad \text{or} \quad q_t = q - \frac{1}{\frac{1}{q} + k_2 t} \quad (6)$$

where k_2 (min^{-1}) is the rate constant of second order adsorption. The kinetic model parameters can be obtained by NLRA. The fitting of this adsorption model to the experimental data was very satisfactory as is shown in Fig.4; this can be proved by the corresponding SEE-values presented in Table 2. The parameters k_2 and q of this model are presented in the same Table 2. The MB maximum amount adsorbed vs. the different adsorption materials, as represented by the parameter q value, estimated for the pretreated wheat straw was significantly higher than the value corresponding to the untreated

Table 3: Parameters of intraparticle kinetic model for Methylene Blue adsorption on pretreatment wheat straw.

Pretreatment	c (mg g^{-1})	k_p ($\text{mg g}^{-1} \text{min}^{-0.5}$)	SEE
Untreated	0.35	0.3437	0.132
160°C, 20min			
Ethanol	2.28	0.5291	0.743
Methanol	1.32	0.4525	0.477
Diethylene glycol	1.71	0.5554	0.558
Acetone	2.07	0.6027	0.721
Butanol	1.53	0.4571	0.512
160°C, 40min			
Ethanol	1.54	0.5755	0.598
Methanol	1.68	0.4675	0.533
Diethylene glycol	3.28	0.6473	1.018
Acetone	1.10	0.6645	0.682
Butanol	1.24	0.5772	0.525
180°C, 20min			
Ethanol	-1.23	0.7259	0.448
Methanol	1.05	0.5403	0.411
Diethylene glycol	3.13	0.5670	0.967
Acetone	-0.82	0.8265	0.458
Butanol	-0.39	0.6520	0.397

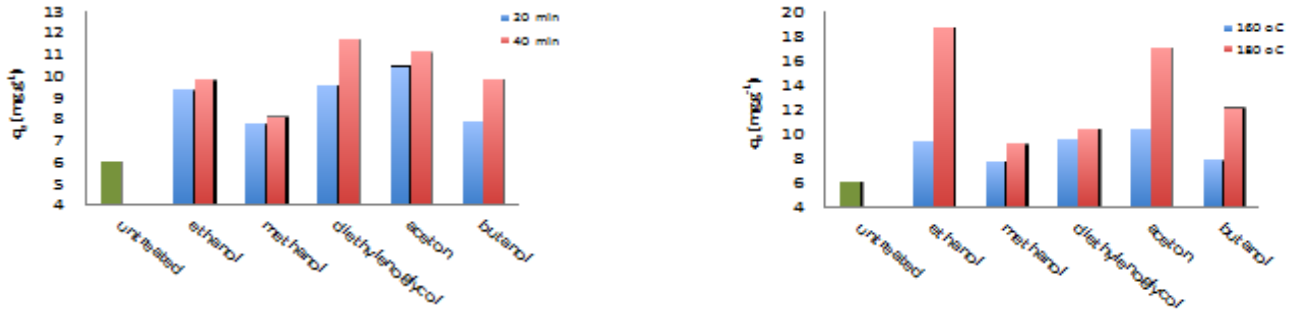


Fig. 5: Kinetic parameter q_t according to the second order model of MB adsorption on modified wheat straw at 160 °C for 20 min and 40 (left) and at 160 and 180 °C for 40 min (right).

sample (see Table 2 and Fig. 5). The possibility of intra-particle diffusion was explored by using the intra-particle diffusion model [23]:

$$q_t = c + k_p \cdot \sqrt{t} \quad (7)$$

where q_t is the amount of MB adsorbed at time t , c is a constant (mg g^{-1}) and k_p is the intra-particle diffusion rate constant in $\text{mg g}^{-1} \text{min}^{-0.5}$. In Table 3 the parameters of intra-particle diffusion model are presented. Tables 3 presents the estimated the intra-particle diffusion kinetic model parameter values and the corresponding SEE values for the experimental data obtained in the present study. In Fig. 6, the intra-particle diffusion kinetic model parameter k_p values estimated for MB adsorption on untreated and pretreated wheat straw and are given. The k_p values for pretreated straw are significantly higher that the value for untreated material. The highest k_p value was obtained in the case of acetone treated straw.

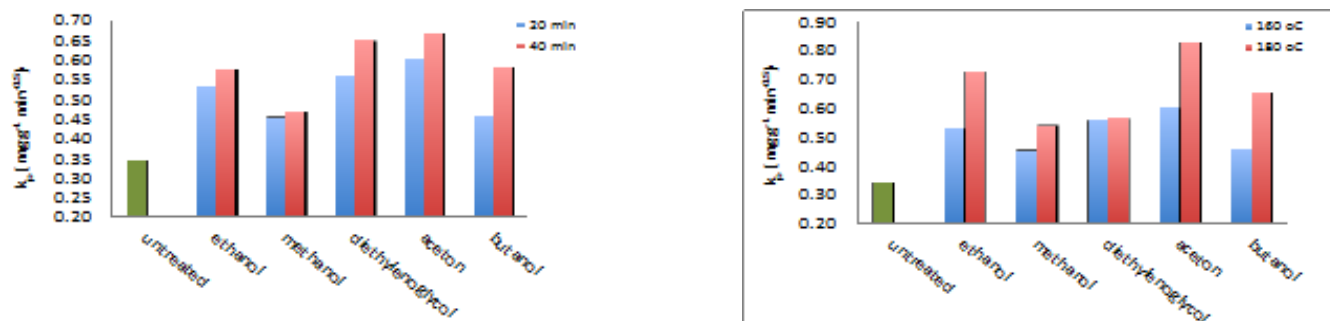


Fig. 6: Kinetic parameter k_p according to the intraparticle diffusion model of MB adsorption on modified wheat straw at 160 °C for 20 min and 40 (left) and at 160 and 180 °C for 40 min (right).

4. Conclusion

According to the above results, organosolv treatment of the wheat straw enhances considerably the materials adsorption properties as regards basic dyes cleaning, like MB, from aquatic environment. Thus, this low-cost widely available material could be used as an alternative adsorbent to commercial activated carbons. The adsorption kinetic data were found to follow the pseudo-second-order kinetic model. Nevertheless, the intra-particle diffusion model was also applicable giving a maximum adsorption rate constant k_p equal to 0.827 as regards wheat straw pretreated with acetone at 180 °C for 20 min; this modified material is appropriate for fast adsorption processes. On the other hand, the isotherm results recommend the use of diethylene glycol pretreated wheat straw, at 160 °C for 20 min, for high adsorption capacity $q_m = 31.7$ mg/g. The decision as regards the use of a specific solvent for the wheat straw pretreatment must be based on the priorities of each adsorption technological application.

Acknowledgements

Financial support by the Research Centre of the University of Piraeus is kindly acknowledged.

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