

Development and Characterization of Mechanically Alloyed and Sintered (Al-7wt.%Si)-2wt.%VB Composites

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Abstract – Vanadium boride (VB) particulate reinforced Al-7 wt.% Si based metal matrix composites (MMC) were synthesized using mechanical alloying (MA) and pressureless sintering. (Al- 7 wt. % Si)-2 wt.% VB blends were mechanically alloyed for 4h in a high energy ball mill. Particle size measurement, Brunauer-Emmett-Teller (BET) surface area analysis, scanning electron microscopy (SEM) investigation and thermal analysis were conducted to characterize the mechanically alloyed powders. As-blended and mechanically alloyed powders were compacted in an uniaxial hydraulic press with a pressure of 450 MPa and green compacts were sintered at 570°C under Ar gas flowing conditions. Microstructural and phase characterizations of the sintered samples were carried out using optical microscope (OM), SEM and X-ray diffractometer (XRD). Physical and mechanical properties of the sintered composites were investigated in terms of density measurements, microhardness measurements and wear rate. MA enhances the physical and mechanical properties of the composites. (Al-7 wt.% Si)-2wt.% VB MA'd for 4 h had relative density value of 95.55%, microhardness value of 1.04±0.11 GPa and wear rate of 1.42×10⁻⁵ mm³/mm.

Keywords: Al-Si based metal matrix composites, Vanadium boride, Mechanical alloying, Pressureless sintering

1. Introduction

Aluminium based MMCs have been used in many areas such as aerospace, aircraft, automotive, and other industrial applications due to their low density, high strength, high elastic modulus, high wear and corrosion resistances and good thermal stabilities [1-3].

Al-based MMCs have been usually fabricated via liquid-phase production techniques such as stir casting, squeeze casting, etc. However, it is possible to fabricate MMCs by solid-state production techniques especially powder metallurgy [4]. Mechanical alloying (MA) which is a high energy ball milling process is a novel part of the powder metallurgy. In MA, components are subjected to repeated cold welding, fracturing and rewelding due to the collisions of the balls in a high-impact vial environment and hence homogeneous distribution can be achieved [5].

Carbides, nitrides, oxides and borides (TiC, SiC, ZrC, Si₃N₄, ZrO₂, Al₂O₃, TiB₂, ZrB₂ etc.) are used as reinforcement materials for Al-based MMCs [6,9-10]. These particulate reinforcement materials improve the mechanical properties of the composite materials [3]. Amongst them, vanadium boride (VB) has high melting point, good wear and corrosion resistance, high hardness, high electrical and thermal conductivities and high chemical stability. Therefore, VB can be used as reinforcement material for Al-based MMCs to improve their hardness and wear resistance [7,8].

2. Experimental Procedure

In this study, the starting materials were elemental aluminium (Al) powders (Alfa Aesar™, 99.5% purity, 12 µm) and silicon (Si) powders (Alfa Aesar™, 99.99% purity, <20 µm). Al and 7wt. % Si (Al7Si) based metal matrix alloy was reinforced with 2wt. % commercial vanadium boride (VB) (Alfa Aesar™, 99.5% purity, ≤44 µm) particles.

Powders were mixed with 2wt.% stearic acid (CH₃(CH₂)₁₆COOH) (ZAG, 99.5% purity) which is a process control agent (PCA) to prevent excessive cold welding and agglomeration of the powders into a hardened steel vial. Powders were loaded into vial in a glove-box (Plaslabs™) by evacuating and filling with high purity Ar gas (Linde™, 99.999% purity) using

a 7/1 ball-to-powder weight ratio. Blended powders were mechanically alloyed in a high energy ball mill (Spex™ 8000D Mixer/Mill, 1200 rpm) for 4 h.

Phase analyses of the as-blended and MA'd powders were performed by using a Bruker™ D8 Advanced Series X-ray diffractometer (XRD) with CuK α radiation (35 kV, 40mA, 2 θ range of 10–90° with a scan rate of 2°/min). Microstructural investigations of powders were performed using JEOL™-6000 Neoscope model scanning electron microscope (SEM). Particle size analyses (PSA) of the powders were conducted with a NanoFlex™ particle sizer. Zeta potentials of the particles were changed from ~pH=5 to pH=9 with Stabino™ with NaOH titrations to disperse the Al powders in water media. Also, Brunauer-Emmett-Teller(BET) surface area analysis was conducted to determine the surface area of the MA'd powders. Thermal analysis was conducted using a TA™ Instruments SDT Q600 differential scanning calorimeter (DSC) to determine the sintering temperature of the MA'd samples.

After the characterization investigations, powders were compacted using a MSE™ uniaxial hydraulic press with 450 MPa. PCA was removed from the bulk samples by heating them up to 420 °C under Ar atmosphere in a MTI™ tube furnace. After the debinding process, samples were sintered at 570 °C with a heating and cooling rate of 5°C/min in a Linn™ HT-1800 high-temperature controlled-atmosphere furnace under vacuum and Ar atmosphere.

XRD analyses were conducted to determine the phases of the sintered samples. Microstructural investigations were performed using Nikon™ Eclipse L150 model optical microscope (OM). Densities of the samples were calculated using the Archimedes method. Hardness measurements of the composites were carried out in a Shimadzu™ Vickers microhardness tester under a load of 100 g for 10 s. Sliding wear tests conducted with a Tribotech™ model tribotester using with a 100Cr6 steel ball (ϕ 6 mm diameter) under 3 N loading (sliding speed: 10 mm/s, stroke length: 5 mm, total sliding distance: 25000 mm). The results in the study were repeated two times in order to eliminate the experimental and individual errors.

3. Results and Discussion

XRD patterns of the as-blended and 4 h of MA'd Al-7 wt.% Si-2wt.% VB powders and their sintered samples are shown in Figure 1(a) and (b). XRD results verified the presence of the Al, Si and VB phases in the powder and bulk systems. There are no secondary phases and intermetallics between the Al, Si and VB phases, or Fe impurity worn from the milling vials/balls during the mechanical alloying, within the detection limit of diffractometer (≥ 2 wt.% of the overall sample). Crystallite sizes and lattice strains of the dominant Al phase in the powders were calculated by the TOPAS software using the XRD patterns of the powders. Crystallite sizes decreased and lattice deformations increased with increasing MA time. Crystallite sizes of the as-blended and MA'd powders are 407.10 nm and 67.93 nm, respectively. Besides, lattice strains change from 0.050% to 0.326% by the effect of MA.

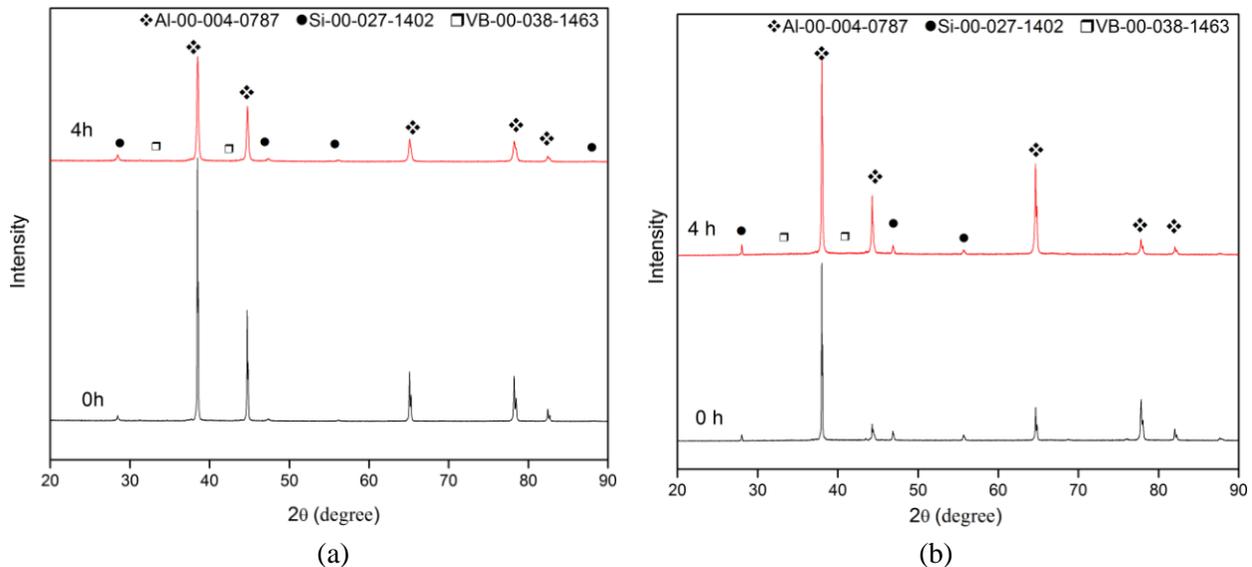


Fig. 1: XRD patterns of the as-blended and 4h of MA'd Al-7wt.% Si-2wt.% VB (a) powders, and (b) their sintered samples.

SEM images show that 4 h of MA'd powders have different morphology from the as-blended ones, as seen in Figure 2. Ductile Al powders transformed to flaky-shaped and equiaxed-shaped structures due to the mechanical impacts in the milling environment. Subsequently, Si and VB particles could be easily embedded into the Al matrix.

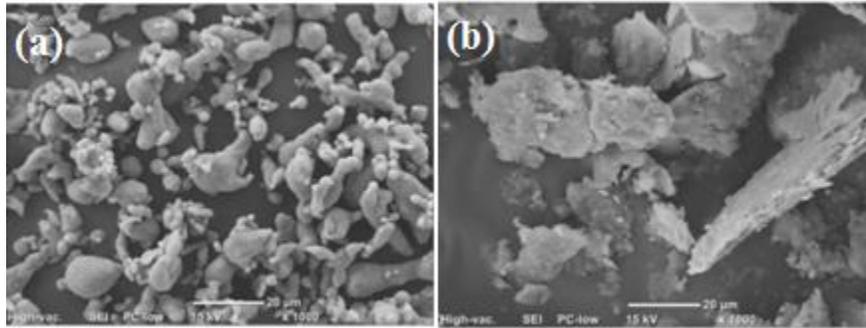


Fig. 2: SEM images of the (a) as-blended and (b) 4h of MA'd Al-7wt.% Si-2wt.% VB powders.

Particle sizes of the powders were determined by using laser diffraction technique. Particle size of the 4h of MA'd powders decreased to 0.376 μm. Bimodal particle size distribution is seen in Figure 3. Results of the BET calculations show that surface area of the powders are about 6.58 m²/g.

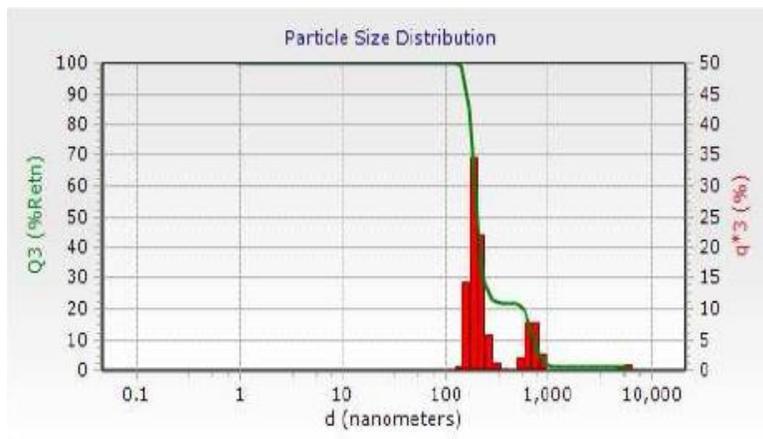


Fig. 3: Particle size distribution of the 4h of MA'd Al-7wt.% Si-2wt.% VB powders.

Thermal analysis was conducted to determine the sintering temperature of the mechanically alloyed samples (Figure 4). The endothermic peak at 578.89°C shows that the Si contributed to the Al structure and shifted the melting temperature to nearly eutectic temperature. Therefore, 570°C is selected as the sintering temperature to perform solid-state sintering.

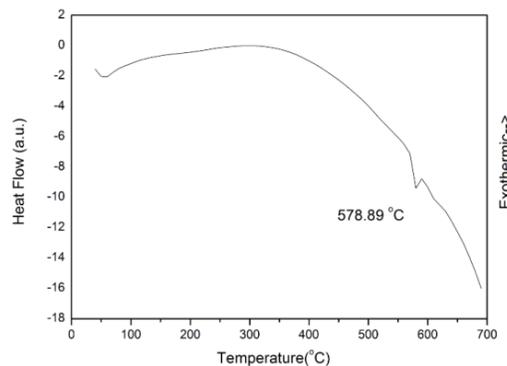


Fig. 4: DSC scan of the 4 h of MA'd Al-7wt.% Si-2wt.% VB powders.

From the optical microscope images in Figure 5, there is not a homogeneous distribution of the particles in the microstructure of the as-blended and sintered sample due to the clustering of the particles (Figure 5(a)). During MA, Si and VB phases incorporated into the Al matrix and a homogeneous microstructure was obtained (Figure 5(b)).

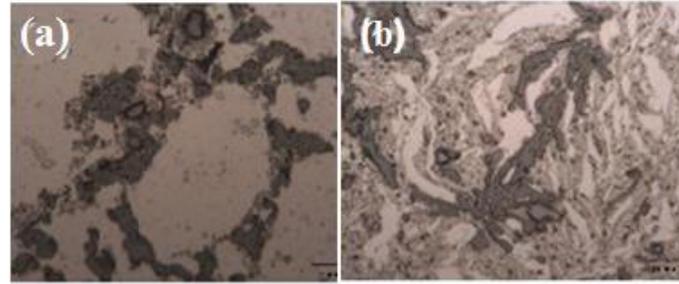


Fig. 5: OM images of the sintered Al-7wt.% Si-2wt.% VB composites originated from: (a) as-blended (1000x) powders and (b) 4 h of MA'd powders (1000x).

Relative density and microhardness results of the as-blended or MA'd and sintered samples are given at Table 1. Measured densities showed that MA'd and sintered samples reached to 95.55% of the theoretical density. Moreover, the increase in the microhardness value of the MA'd and sintered sample is nearly twice of the as-blended and sintered sample (from 0.48 GPa to 1.04 GPa). MA'd and sintered Al-7wt.% Si-2wt.% VB composite has the wear rate of $1.42 \times 10^{-5} \text{ mm}^3/\text{N.m}$. Also, OM and SEM images of the worn surfaces belonging to the 4 h of MA'd and sintered Al-7wt.% Si-2wt.% VB composite are shown in Figure 6(a) and (b), respectively.

Table 1: Density and microhardness values of the as-blended or 4h of MA'd and sintered Al-7wt.% Si-2 wt.% VB composites.

MA time	Theoretical density (g/cm ³)	Archimedes density (g/cm ³)	Relative density (%)	Vickers microhardness (GPa)
as-blended	2.69	2.487	92.25	0.48±0.06
4 h		2.576	95.55	1.04±0.11

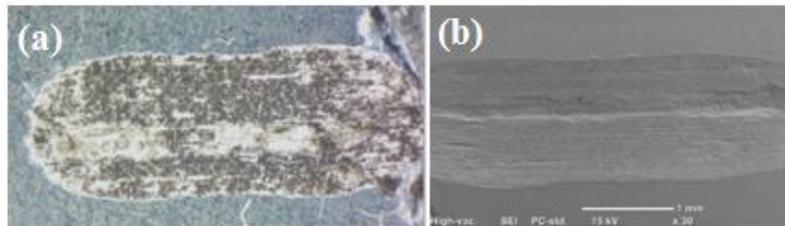


Fig. 6: (a) OM and (b) SEM (30x) images of the worn surfaces of the 4 h of MA'd and sintered Al-7wt.% Si-2wt.% VB composite.

4. Conclusion

Mechanical and physical properties of the VB particulate reinforced Al-7wt.% Si MMCs were improved with mechanical alloying process probably due to the homogeneous distribution of the powder particles. Relative density and microhardness values of the MA'd and sintered sample reached to 95.55% and 1.04 GPa, respectively. Also, MA'd and sintered sample had the wear rate of $1.42 \times 10^{-5} \text{ mm}^3/\text{N.m}$.

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